

Footing Reinforcing Design (F-2) - Includes Uplift Strength Check:

$$f'_c := 3000 \text{ psi} \quad E := 29000 \text{ ksi} \quad \lambda := 1.0 \quad F_y := 60 \text{ ksi}$$

$$W := 6 \text{ ft} \quad L := 4 \text{ ft} \quad T := 10 \text{ in} \quad C_{top} := 2 \cdot \text{in} \quad C_{bottom} := 3 \text{ in}$$

$$Base_W := 12 \text{ in} \quad Base_L := 12 \text{ in} \quad \rho_{concrete} := 145 \text{ pcf}$$

$$\text{Loading:} \quad P_{Dead} := 1 \text{ kip} \quad P_{Soil} := 200 \text{ psf} \quad P_{Wind} := -7 \text{ kip}$$

$$P_{Self} := \rho_{concrete} \cdot W \cdot L \cdot T + P_{Soil} \cdot W \cdot L - P_{Soil} \cdot Base_W \cdot Base_L = 7.5 \text{ kip}$$

$$\text{Max Soil Bearing Pressure:} \quad \sigma_{max} := \begin{bmatrix} 3000 \text{ psf} \\ 3000 \text{ psf} \\ 3000 \text{ psf} \end{bmatrix} \quad bearingCapacity := \sigma_{max} \cdot W \cdot L = \begin{bmatrix} 72 \\ 72 \\ 72 \end{bmatrix} \text{ kip}$$

ASD Load Combinations:

Uplift Resisting Weight:

$$P_{asd} := \begin{bmatrix} P_{Dead} + P_{Self} \\ P_{Dead} + P_{Self} + P_{Wind} \\ 0.6 \cdot (P_{Dead} + P_{Self}) + 0.6 \cdot P_{Wind} \end{bmatrix} = \begin{bmatrix} 8.5 \\ 1.5 \\ 0.9 \end{bmatrix} \text{ kip} \quad W_r := \begin{bmatrix} P_{Dead} + P_{Self} \\ P_{Dead} + P_{Self} \\ 0.6 \cdot (P_{Dead} + P_{Self}) \end{bmatrix} = \begin{bmatrix} 8.5 \\ 8.5 \\ 5.1 \end{bmatrix} \text{ kip}$$

Footing Reinforcing:

Reinforcing Top:

$$Bar_W := 4 \quad A_{s_W} := A_{bar}(Bar_W) = 0.2 \text{ in}^2 \quad N_{bars_W} := 5 \quad Bar_Spacing(W, N_{bars_W}) = 16.5 \text{ in}$$

$$Bar_L := 4 \quad A_{s_L} := A_{bar}(Bar_L) = 0.2 \text{ in}^2 \quad N_{bars_L} := 4 \quad Bar_Spacing(L, N_{bars_L}) = 14 \text{ in}$$

Reinforcing Bottom:

$$Bar_W := 4 \quad A_{s_W} := A_{bar}(Bar_W) = 0.2 \text{ in}^2 \quad N_{bars_W} := 5 \quad Bar_Spacing(W, N_{bars_W}) = 16.5 \text{ in}$$

$$Bar_L := 4 \quad A_{s_L} := A_{bar}(Bar_L) = 0.2 \text{ in}^2 \quad N_{bars_L} := 4 \quad Bar_Spacing(L, N_{bars_L}) = 14 \text{ in}$$

Steel Depths:

$$\text{Top:} \quad d_W := C_{top} + D_{bar}(Bar_L) + \frac{D_{bar}(Bar_W)}{2} = 2.75 \text{ in}$$

$$d_L := C_{top} + D_{bar}(Bar_W) + \frac{D_{bar}(Bar_L)}{2} = 2.75 \text{ in}$$

$$\text{Bottom:} \quad d_W := T - \left(C_{bottom} + D_{bar}(Bar_L) + \frac{D_{bar}(Bar_W)}{2} \right) = 6.25 \text{ in}$$

$$d_L := T - \left(C_{bottom} + D_{bar}(Bar_W) + \frac{D_{bar}(Bar_L)}{2} \right) = 6.25 \text{ in}$$

Steel Ratios:

$$SteelCheck(\rho_w) := \text{if}(\rho_w > 0, \text{if}(\rho_w > 0.0018, \text{"OK"}, \text{"Not Enough"}), \text{"NA"})$$

Top: $\rho_{W_top} := \frac{A'_{s_W} \cdot N'_{bars_W}}{W \cdot (T - d'_W)} = 0.0019$ $SteelCheck(\rho_{W_top}) = \text{"OK"}$

$$\rho_{L_top} := \frac{A'_{s_L} \cdot N'_{bars_L}}{L \cdot (T - d'_L)} = 0.0023$$
 $SteelCheck(\rho_{L_top}) = \text{"OK"}$

Bottom: $\rho_{W_bottom} := \frac{A_{s_W} \cdot N_{bars_W}}{W \cdot d_W} = 0.0022$ $SteelCheck(\rho_{W_bottom}) = \text{"OK"}$

$$\rho_{L_bottom} := \frac{A_{s_L} \cdot N_{bars_L}}{L \cdot d_L} = 0.0027$$
 $SteelCheck(\rho_{L_bottom}) = \text{"OK"}$

Single Shear:

$$V_n(f'_c, b, d, \rho_w) := \begin{cases} \text{if } \rho_w \geq 0.0018 \\ \left| \begin{array}{l} V_{c1} \leftarrow 2 \cdot \sqrt{\frac{f'_c}{psi}} \cdot psi \cdot b \cdot d \\ V_{c2} \leftarrow 8 \cdot \lambda \cdot (\rho_w)^{\frac{1}{3}} \cdot \sqrt{\frac{f'_c}{psi}} \cdot psi \cdot b \cdot d \\ \text{return } \min\left(\max(V_{c1}, V_{c2}), 5 \cdot \lambda \cdot \sqrt{\frac{f'_c}{psi}} \cdot psi \cdot b \cdot d\right) \end{array} \right. \\ \text{else} \\ \left| \text{return } 0 \text{ kip} \end{cases}$$

$$V_{n_W} := V_n(f'_c, W, d_W, \rho_{W_bottom}) = 49.295 \text{ kip} \quad \phi V_{n_W} := 0.75 \cdot V_{n_W} = 36.971 \text{ kip}$$

$$V_{n_L} := V_n(f'_c, L, d_L, \rho_{L_bottom}) = 32.863 \text{ kip} \quad \phi V_{n_L} := 0.75 \cdot V_{n_L} = 24.648 \text{ kip}$$

Double Shear:

$$V_{c_punching}(W, L, Base_W, Base_L, d) := \begin{cases} \beta \leftarrow \frac{\max(W, L)}{\min(W, L)} \\ b_{o_w} \leftarrow \text{if}(Base_L + d \geq L, 0 \text{ in}, Base_W + d) \\ b_{o_l} \leftarrow \text{if}(Base_W + d \geq W, 0 \text{ in}, Base_L + d) \\ b_o \leftarrow 2 \cdot b_{o_w} + 2 \cdot b_{o_l} \\ \text{if } b_o > 0 \text{ in} \\ \left| \begin{array}{l} \alpha_s \leftarrow 40 \\ \text{return } \min\left(\left(4 \cdot \lambda \cdot \sqrt{\frac{f'_c}{psi}} \cdot psi\right), \left(2 + \frac{4}{\beta}\right) \cdot \lambda \cdot \sqrt{\frac{f'_c}{psi}} \cdot psi, \left(\frac{\alpha_s \cdot d}{b_o} + 2\right) \cdot \lambda \cdot \sqrt{\frac{f'_c}{psi}} \cdot psi\right) \cdot b_o \cdot d \end{array} \right. \\ \text{else} \\ \left| \text{return } 0 \text{ kip} \end{cases}$$

$$\phi V_{c_punching} := 0.75 \cdot V_{c_punching}(W, L, Base_W, Base_L, \min(d_W, d_L)) = 74.97 \text{ kip}$$

Calculate Moment Capacity:

$$M_n(A_{bottom}, N_{bottom}, A_{top}, N_{top}, b, T, d, d', F_y, f_c, E) :=$$

$$\beta_1 \leftarrow \begin{cases} \text{if } f'_c \leq 4000 \text{ psi} \\ 0.85 \\ \text{else if } f'_c \leq 8000 \text{ psi} \\ 0.85 - 0.05 \cdot \frac{(f'_c - 4000 \text{ psi})}{1000 \text{ psi}} \\ \text{else} \\ 0.65 \end{cases}$$

$$A_s \leftarrow A_{bottom} \cdot N_{bottom}$$

$$A'_s \leftarrow A_{top} \cdot N_{top}$$

$$\rho \leftarrow \frac{A_s}{b \cdot d}$$

$$\rho' \leftarrow \frac{A'_s}{b \cdot (T - d')}$$

$$\text{if } \rho \geq 0.0018$$

$$\text{if } \rho - \rho' \geq \frac{\beta_1 \cdot 0.85 \cdot f'_c \cdot d'}{F_y \cdot d} \cdot \frac{87000 \text{ psi}}{87000 \text{ psi} - F_y}$$

$$c \leftarrow \frac{(A_s - A'_s) \cdot F_y}{0.85 \cdot \beta_1 \cdot b \cdot f'_c}$$

$$a \leftarrow \beta_1 \cdot c$$

$$M_n \leftarrow A'_s \cdot F_y \cdot (d - d') + (A_s - A'_s) \cdot F_y \cdot \left(d - \frac{a}{2}\right)$$

$$\text{else}$$

$$c \leftarrow \frac{\sqrt{9 \cdot E^2 \cdot A_s'^2 \downarrow - 6000 \cdot E \cdot A_s \cdot F_y \cdot A_s' \downarrow + 10200 \cdot b \cdot d' \cdot \beta_1 \cdot f'_c \cdot E \cdot A_s' \downarrow + 1000000 \cdot A_s^2 \cdot F_y^2 - 3 \cdot E \cdot A_s' + 1000 \cdot A_s \cdot F_y}}{1700 \cdot b \cdot \beta_1 \cdot f'_c}$$

$$a \leftarrow \beta_1 \cdot c$$

$$M_n \leftarrow 0.85 \cdot f'_c \cdot b \cdot \beta_1 \cdot c \cdot \left(d - \frac{a}{2}\right) \downarrow + A'_s \cdot E \cdot 0.003 \cdot \left(\frac{c - d'}{c}\right) \cdot (d - d')$$

$$\text{else}$$

$$M_n \leftarrow 0 \text{ kip} \cdot \text{ft}$$

$$\text{return } M_n$$

Moment Down Direction:

$$M_{n_W} := M_n(A_{s_W}, N_{bars_W}, A'_{s_W}, N'_{bars_W}, W, T, d_W, d'_W, F_y, f'_c, E) = 51.427 \text{ kip} \cdot \text{ft}$$

$$M_{n_L} := M_n(A_{s_L}, N_{bars_L}, A'_{s_L}, N'_{bars_L}, L, T, d_L, d'_L, F_y, f'_c, E) = 38.141 \text{ kip} \cdot \text{ft}$$

$$\phi M_{n_W_Down} := 0.9 \cdot M_{n_W} = 46.284 \text{ kip} \cdot \text{ft}$$

$$\phi M_{n_L_Down} := 0.9 \cdot M_{n_L} = 34.327 \text{ kip} \cdot \text{ft} \quad P_u := \begin{bmatrix} 1.4 \cdot (P_{Dead} + P_{Self}) \\ 1.2 \cdot (P_{Dead} + P_{Self}) + 1.0 \cdot P_{Wind} \\ 0.9 \cdot (P_{Dead} + P_{Self}) + 1.0 \cdot P_{Wind} \end{bmatrix} = \begin{bmatrix} 11.9 \\ 3.2 \\ 0.65 \end{bmatrix} \text{ kip}$$

Calculating Single Shear Demand:

$$V_{u_W} := \begin{cases} \text{if } \frac{Base_L}{2} + d_W < \frac{L}{2} \\ \left| \frac{P_u \cdot \left(\frac{L}{2} - \left(\frac{Base_L}{2} + d_L \right) \right)}{L} \right| \\ \text{else} \\ 0 \text{ kip} \end{cases} = \begin{bmatrix} 2.913 \\ 0.783 \\ 0.159 \end{bmatrix} \text{ kip} \quad V_{u_L} := \begin{cases} \text{if } \frac{Base_W}{2} + d_L < \frac{W}{2} \\ \left| \frac{P_u \cdot \left(\frac{W}{2} - \left(\frac{Base_W}{2} + d_W \right) \right)}{W} \right| \\ \text{else} \\ 0 \text{ kip} \end{cases} = \begin{bmatrix} 3.925 \\ 1.056 \\ 0.214 \end{bmatrix} \text{ kip}$$

Calculate Punching Shear Demand:

$$V_{u_Punching} := \begin{cases} d \leftarrow \min(d_W, d_L) \\ b_{o_W} \leftarrow \min(Base_W + d, W) \\ b_{o_L} \leftarrow \min(Base_L + d, L) \\ \text{if } b_{o_W} \cdot b_{o_L} > 0 \text{ in}^2 \\ \left| \text{return } P_u - \frac{P_u}{W \cdot L} \cdot (b_{o_W} \cdot b_{o_L}) \right| \\ \text{else} \\ \left| \text{return } 0 \text{ kip} \right| \end{cases} = \begin{bmatrix} 10.753 \\ 2.892 \\ 0.587 \end{bmatrix} \text{ kip}$$

Calculate Factored Moment Demand:

$$M_{u_W} := \frac{P_u \cdot \left(\frac{L}{2} - \frac{Base_L}{2} \right)^2}{2 \cdot L} = \begin{bmatrix} 3.347 \\ 0.9 \\ 0.183 \end{bmatrix} \text{ kip} \cdot \text{ft} \quad M_{u_L} := \frac{P_u \cdot \left(\frac{W}{2} - \frac{Base_W}{2} \right)^2}{2 \cdot W} = \begin{bmatrix} 6.198 \\ 1.667 \\ 0.339 \end{bmatrix} \text{ kip} \cdot \text{ft}$$

Check Footing Shear Capacity:

$$V_{u_W} = \begin{bmatrix} 2.913 \\ 0.783 \\ 0.159 \end{bmatrix} \text{ kip} \quad V_{u_L} = \begin{bmatrix} 3.925 \\ 1.056 \\ 0.214 \end{bmatrix} \text{ kip} \quad V_{u_Punching} = \begin{bmatrix} 10.753 \\ 2.892 \\ 0.587 \end{bmatrix} \text{ kip}$$

$$\phi V_{n_W} = 36.971 \text{ kip}$$

$$\phi V_{n_L} = 24.648 \text{ kip}$$

$$\phi V_{c_punching} = 74.97 \text{ kip}$$

$$\frac{V_{u_W}}{\phi V_{n_W}} = \begin{bmatrix} 0.079 \\ 0.021 \\ 0.004 \end{bmatrix}$$

$$\frac{V_{u_L}}{\phi V_{n_L}} = \begin{bmatrix} 0.159 \\ 0.043 \\ 0.009 \end{bmatrix}$$

$$\frac{V_{u_Punching}}{\phi V_{c_punching}} = \begin{bmatrix} 0.143 \\ 0.039 \\ 0.008 \end{bmatrix}$$

$$shearDesignRatio := \max \left(\frac{V_{u_W}}{\phi V_{n_W}}, \frac{V_{u_L}}{\phi V_{n_L}}, \frac{V_{u_Punching}}{\phi V_{c_punching}} \right) = 0.159$$

Check Footing Moment Capacity:

$$M_{u_W} = \begin{bmatrix} 3.347 \\ 0.9 \\ 0.183 \end{bmatrix} \text{ kip}\cdot\text{ft}$$

$$M_{u_L} = \begin{bmatrix} 6.198 \\ 1.667 \\ 0.339 \end{bmatrix} \text{ kip}\cdot\text{ft}$$

$$\phi M_{n_W_Down} = 46.284 \text{ kip}\cdot\text{ft}$$

$$\phi M_{n_L_Down} = 34.327 \text{ kip}\cdot\text{ft}$$

$$\frac{M_{u_W}}{\phi M_{n_W_Down}} = \begin{bmatrix} 0.072 \\ 0.019 \\ 0.004 \end{bmatrix}$$

$$\frac{M_{u_L}}{\phi M_{n_L_Down}} = \begin{bmatrix} 0.181 \\ 0.049 \\ 0.01 \end{bmatrix}$$

$$momentDesignRatio := \max\left(\frac{M_{u_W}}{\phi M_{n_W_Down}}, \frac{M_{u_L}}{\phi M_{n_L_Down}}\right) = 0.181$$

Bearing Check:

ASD Bearing Force: $P_{asd} = \begin{bmatrix} 8.5 \\ 1.5 \\ 0.9 \end{bmatrix} \text{ kip}$

Resisting Force: $W_r = \begin{bmatrix} 8.5 \\ 8.5 \\ 5.1 \end{bmatrix} \text{ kip}$

$$bearingCheck := \begin{array}{l} i \leftarrow \text{ORIGIN} \dots \text{rows}(P_{asd}) - 1 \\ check \leftarrow 0 \\ \text{for } j \in i \\ \quad \text{if } P_{asd_j} < 0 \text{ kip} \\ \quad \quad \quad check_j \leftarrow \frac{-1 \cdot (P_{asd_j} - W_{r_j})}{W_{r_j}} \\ \quad \text{else} \\ \quad \quad \quad check_j \leftarrow \frac{P_{asd_j}}{bearingCapacity_j} \\ \text{return } check \end{array} = \begin{bmatrix} 0.118 \\ 0.021 \\ 0.013 \end{bmatrix}$$

Check For Uplift On Footing:

$$\text{Service Level: } P_{asd} = \begin{bmatrix} 8500 \\ 1500 \\ 900 \end{bmatrix} \text{ lbf} \quad \text{Strength Level: } P_u = \begin{bmatrix} 11900 \\ 3200 \\ 650 \end{bmatrix} \text{ lbf}$$

Note All values are positive, so no uplift from ASD Load Combinations

$$\text{Force Resisting Strength Level Uplift Forces: } W_r := \begin{bmatrix} 1.4 \cdot (P_{Dead} + P_{Self}) \\ 1.2 \cdot (P_{Dead} + P_{Self}) \\ 0.9 \cdot (P_{Dead} + P_{Self}) \end{bmatrix} = \begin{bmatrix} 11.9 \\ 10.2 \\ 7.65 \end{bmatrix} \text{ kip}$$

Check for tension loads at top of footing:

$$P_t := P_u - W_r = \begin{bmatrix} 0 \\ -7000 \\ -7000 \end{bmatrix} \text{ lbf}$$

Check Factored Uplift Shear:

$$V_{u_W} := \min \left(\frac{P_t}{2} - \frac{P_t \cdot (T - d'_L)}{L} \right) = -2.443 \text{ kip}$$

Note: don't use the bearing plate dimensions for shear or moment capacity calculations because there's no base plate on the bottom of the footing.

$$V_{u_L} := \min \left(\frac{P_t}{2} - \frac{P_t \cdot (T - d'_W)}{W} \right) = -2.795 \text{ kip}$$

Calculate Factored Punching Shear:

$$d_p := \min((T - d'_W), (T - d'_L)) = 7.25 \text{ in}$$

$$V_{u_Punching} := \min \left(P_t - \frac{P_t}{W \cdot L} \cdot (d_p^2) \right) = -6.894 \text{ kip}$$

Calculate Factored Moment:

$$M_{u_W} := \min \left(\frac{L \cdot P_t}{8} \right) = -3.5 \text{ kip} \cdot \text{ft}$$

$$M_{u_L} := \min \left(\frac{W \cdot P_t}{8} \right) = -5.25 \text{ kip} \cdot \text{ft}$$

Uplift Check:

$$\text{upliftCheck} := \begin{array}{l} i \leftarrow \text{ORIGIN} \dots \text{rows}(P_u) - 1 \\ \text{check} \leftarrow 0 \\ \text{for } j \in i \\ \quad \text{if } P_{u_j} - W_{r_j} < 0 \text{ kip} \\ \quad \quad \text{check}_j \leftarrow \frac{-1 \cdot (P_{u_j} - W_{r_j})}{W_{r_j}} \\ \quad \text{else} \\ \quad \quad \text{check}_j \leftarrow 0.0 \\ \text{return check} \end{array} = \begin{bmatrix} 0 \\ 0.686 \\ 0.915 \end{bmatrix}$$

Single Shear Capacity - Up:

$$V_{n_W} := V_n(f'_c, W, T - d'_W, \rho_{W_top}) = 57.182 \text{ kip} \quad \phi V_{n_W} := 0.75 \cdot V_{n_W} = 42.887 \text{ kip}$$

$$V_{n_L} := V_n(f'_c, L, T - d'_L, \rho_{L_top}) = 38.121 \text{ kip} \quad \phi V_{n_{L_up}} := 0.75 \cdot V_{n_L} = 28.591 \text{ kip}$$

$$\phi V_{c_punching_up} := 0.75 \cdot V_{c_punching}(W, L, 0 \text{ in}, 0 \text{ in}, \min(T - d'_W, T - d'_L)) = 34.548 \text{ kip}$$

$$\text{if}(-1 \cdot V_{u_W} \leq \phi V_{n_W}, \text{"OK"}, \text{"FAIL"}) = \text{"OK"} \quad -1 \cdot \frac{V_{u_W}}{\phi V_{n_W}} = 0.057$$

$$\text{if}(-1 \cdot V_{u_L} \leq \phi V_{n_L}, \text{"OK"}, \text{"FAIL"}) = \text{"OK"} \quad -1 \cdot \frac{V_{u_L}}{\phi V_{n_L}} = 0.113$$

$$\text{if}(-1 \cdot V_{u_Punching} \leq \phi V_{c_punching}, \text{"OK"}, \text{"FAIL"}) = \text{"OK"} \quad -1 \cdot \frac{V_{u_Punching}}{\phi V_{c_punching}} = 0.092$$

Moment Capacity - Up Direction:

$$M_{n_W} := M_n(A'_{s_W}, N'_{bars_W}, A_{s_W}, N_{bars_W}, W, T, T - d'_W, T - d_W, F_y, f'_c, E) = 73.668 \text{ kip} \cdot \text{ft}$$

$$M_{n_L} := M_n(A'_{s_L}, N'_{bars_L}, A_{s_L}, N_{bars_L}, L, T, T - d'_L, T - d_L, F_y, f'_c, E) = 54.122 \text{ kip} \cdot \text{ft}$$

$$\phi M_{n_W} := 0.9 \cdot M_{n_W} = 66.301 \text{ kip} \cdot \text{ft} \quad \phi M_{n_L} := 0.9 \cdot M_{n_L} = 48.71 \text{ kip} \cdot \text{ft}$$

$$\text{if}(-1 \cdot \min(M_{u_W}) \leq \phi M_{n_W}, \text{"OK"}, \text{"FAIL"}) = \text{"OK"} \quad -1 \cdot \frac{M_{u_W}}{\phi M_{n_W}} = 0.053$$

$$\text{if}(-1 \cdot \min(M_{u_L}) \leq \phi M_{n_L}, \text{"OK"}, \text{"FAIL"}) = \text{"OK"} \quad -1 \cdot \frac{M_{u_L}}{\phi M_{n_L}} = 0.108$$

Footing Bearing Analysis:

Bearing Code Check = 0.92

P = -7.00 kips vs 7.65 kips

For 0.9 Dead + 1.0 Wind

Footing Shear Analysis:

Shear Code Check = 0.20

Vu = -6.89 kips vs 34.55 kips

For 0.9 Dead + 1.0 Wind

Footing Moment Analysis:

Moment Code Check = 0.18

Mu = 6.20 kip-ft vs 34.33 kip-ft

For 1.4 Dead